
TASK

Official Newsletter of the Southern Ontario Glider Group Inc.

Volume 16 Issue 3

June 2000



Inside This Issue:

- Getting the Bird
- History Page
- Thermal Seeking
- Membership List
- Events Calendar
- For Sale



IF YOU BUILD IT.....

If you build it in time for the first contest, then that in itself should be worth bonus points.....
Got mine! How about you guys? See the CD for the special offers in the month of June.

The birds have flown! Most of the fledgling Birds of Time have fled the nest and are fending for themselves in contests and in search of thermals.

May has been a busy month, firstly a trip to England – with flying visits to the Shuttleworth Collection and the Aerospace Museum at Cosford, visits to several Pubs and a short course in grand prix racing. (How fast can you circle a round-a-bout three times before exiting on the right road?). Then another race to get the B-O-T ready for flying. Just made it in time for the first of the single design contests (with a little help from the weather).

Initial impressions of the Bird of Time are very positive. Although, a note of caution – screw up on the release and you can lose 300' in two seconds flat and then may have to bleed off speed with a low level inverted pass across the flying field – forget which way is up and all that will be left is feathers! But get this baby set up right and you will have many hours of fun.

Ever have that horrid sinking feeling that your million dollar aircraft has just taken a mind of its own and refuses to respond to your commands? Good! That makes at least two of us. Last Saturday my Windfree did just that: ignored any commands from the transmitter and just hopped a thermal and sailed away. Oh serendipity! that was the phrase that came to mind. However sometimes the Sailplane gods smile kindly on the lesser mortals, the Windfree sailed over the woods and into the distance – no one would have guessed that it was flying free – and so the long search began. With the help of Ottokar K. a wide area was searched but no sign of any plane. Lunchtime rolled round, and having snatched a bite, the search was resumed – concentrating in the area of a tree farm. Again the search yielded no success. The ground search was called off at 3.00 pm and spirits were definitely low. Then when all else fails, inspiration takes over – why not check things out from above – so a quick trip to John C. Munro Airport, grab a quick flight in a small plane (and I mean small) and in less than twenty minutes what was lost is located (over a quarter of a mile further away than first thought) and suddenly the world seems a much brighter place. Recovery of the plane was straightforward, no damage at all except dud receiver batteries, and a massive donation of blood to the Mosquito Food Bank. Moral of the story, double check your batteries, don't think that charging and cycling them means that they hold a charge and don't use any but the best.

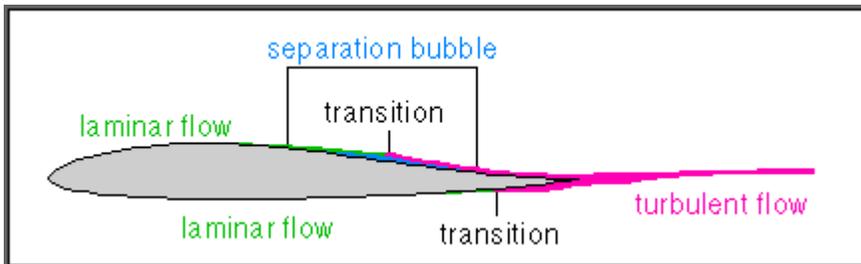
Turbulators by Martin Hepperle

Introduction

The additional drag, which arises from laminar separation bubbles, can be eliminated, by avoiding them or by reducing their size, using one of the following measures:

1. natural transition by shaping the airfoil geometry in such a way that the transition occurs already in front of the main pressure recovery region, where the bubble might occur, or by
2. forced transition by artificial disturbances, e.g. a turbulator. This device will usually be attached just before the region of laminar separation and has to introduce enough disturbances to cause transition into the turbulent state, before the laminar separation can occur.

For the low Reynolds numbers of model aircraft, forced transition by means of a turbulator seems to be more recommendable. A small drag increase in the high-speed regime is the cost which has to be paid for the bigger improvements at low flight speed. It is not a result of a bad design, when an airfoil needs a turbulator for best performance - at least not at Reynolds numbers below 1 million.



The turbulator causes transition without laminar separation.

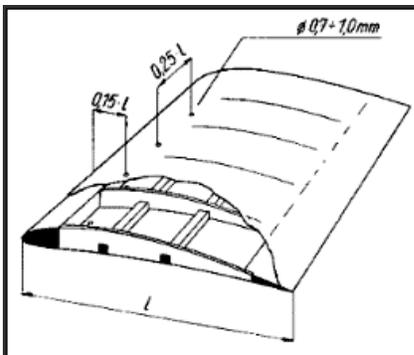
Mechanical Turbulators

A mechanical turbulator consists of a modification of the airfoil shape, which causes large local gradients in the shear stress of the fluid, which finally cause transition. It can be attached to the surface as a straight tape strip (also called a 2D turbulator) or it can be distributed in a certain area like zigzag tapes or single bumps, spaced equally. A different possibility, which has been used on free flight models, is a wire, which is mounted on small struts in front of the leading edge. This device is less sensitive to changes in angle of attack, but causes larger additional drag.

Typical values for turbulator height on model aircraft range from 0.2 for higher Reynolds numbers to more than 1 mm for free flight models (see [below for an approximate method](#) to find a suitable turbulator height). Zigzag tape is used on full-scale gliders too, and is available from some manufacturers in different sizes.

Pneumatic Turbulators

Pneumatic turbulator for free flight models



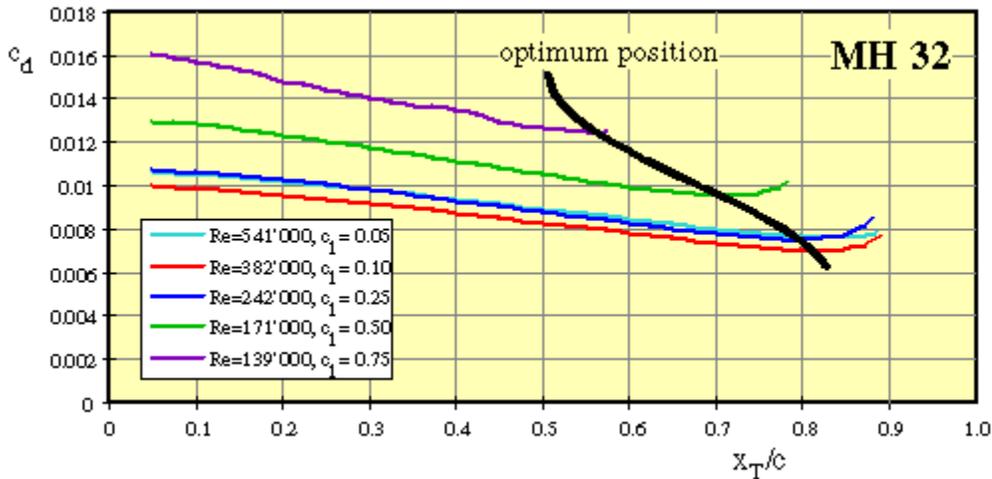
A different method to cause transition is the so-called pneumatic turbulator, which may even be controlled - either automatically or by a remote control system. Such devices are well known for years and have been used in man carrying aircraft as well as in model aircraft.

A pneumatic turbulator consists of an array of holes in the wing surface, which are used to eject a small amount of air into the boundary layer. If the amount of air is sufficient, the resulting turbulent wedges cause transition downstream of the holes. The flow through the holes can be driven by [pitot tubes](#) or by the pressure difference between upper and lower wing surface. By a clever selection of the chord position for the holes in the lower surface, the quantity of the airflow can be controlled

automatically, depending on the angle of attack. A drawback of pneumatic turbulators is their sensitivity to dust and dirt, which may fill the small holes, and the amount of work to install such a device.

Placing the Turbulator

The optimum turbulator should avoid laminar separation bubbles without increasing the drag. Unfortunately, on most high performance, low Reynolds number airfoils; the position of the separation bubble tends to move when the lift coefficient changes. Also the Reynolds number is depending on the lift coefficient: circling in a thermal requires high lift coefficients and low Reynolds numbers, whereas cruising at high speed leads to high Reynolds numbers at low lift coefficients. Thus a fixed turbulator will be a compromise: when it is located forward, to avoid bubbles at higher lift coefficients, it will create additional drag at lower lift coefficients, and when it is located more rearwards, it will be ineffective at higher lift coefficients.

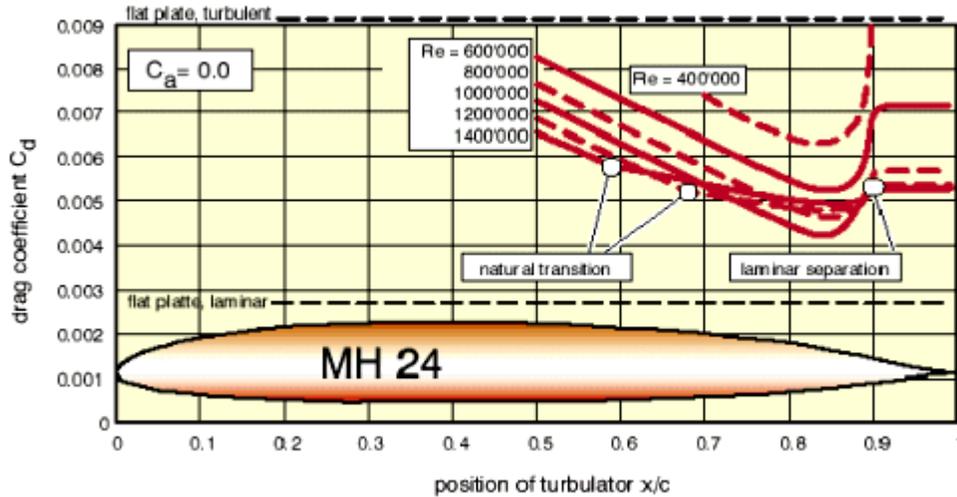


Calculated drag coefficient of the MH 32 for 5 different lift coefficient/Reynolds number combinations. Transition has been fixed at different x/c locations.

The figure above shows the results of a numerical experiment. For different combinations of Reynolds number and lift coefficient, corresponding to a typical F3B sailplane, the drag coefficient has been calculated. The transition has been forced to occur at different stations x/c , starting at $x/c = 5\%$. Picking the curve for $Re = 171'000, Cl = 0.5$ shows, that the drag coefficient decreases steadily, while we move the turbulator rearwards, until we reach a point where the curve levels out. This is the location, where the separation bubble starts. Moving the turbulator further towards the trailing edge leads to an increase in C_d : the turbulator is simply in or even behind the bubble and has no effect anymore. A useable compromise would be to place the turbulator somewhere between 60% and 80% of the chord length, say at 70%. If you were very picky, you would have to choose different positions along the span, depending on local Reynolds number and lift coefficient - but that might generally be considered harmfully close to splitting your hair.

In general, it is possible to design airfoils so, that the separation bubble stays at the same location, but this location has to be chosen according to the low Reynolds number case (close to $x/c = 50\%$ for the above example), resulting in higher drag at higher Reynolds numbers.

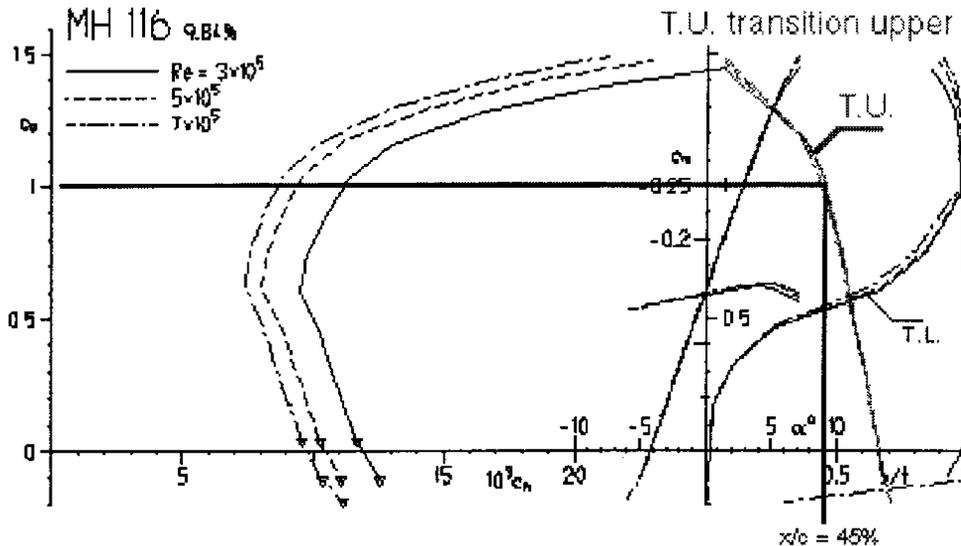
Turbulators are helpful not only at very low Reynolds numbers - even on full scale sailplanes turbulators are widely used to improve their performance. The figure below shows the results of a numerical study to find the optimum turbulator position on the MH 24 pylon racing airfoil, which operates at Reynolds numbers around 1 Million.



Calculated drag coefficient of the MH 24 for different Reynolds numbers. The optimum position seems to be at 84% of the chord. The drag of the airfoil comes close to the flat plate with completely laminar flow.

Sizing the Turbulator

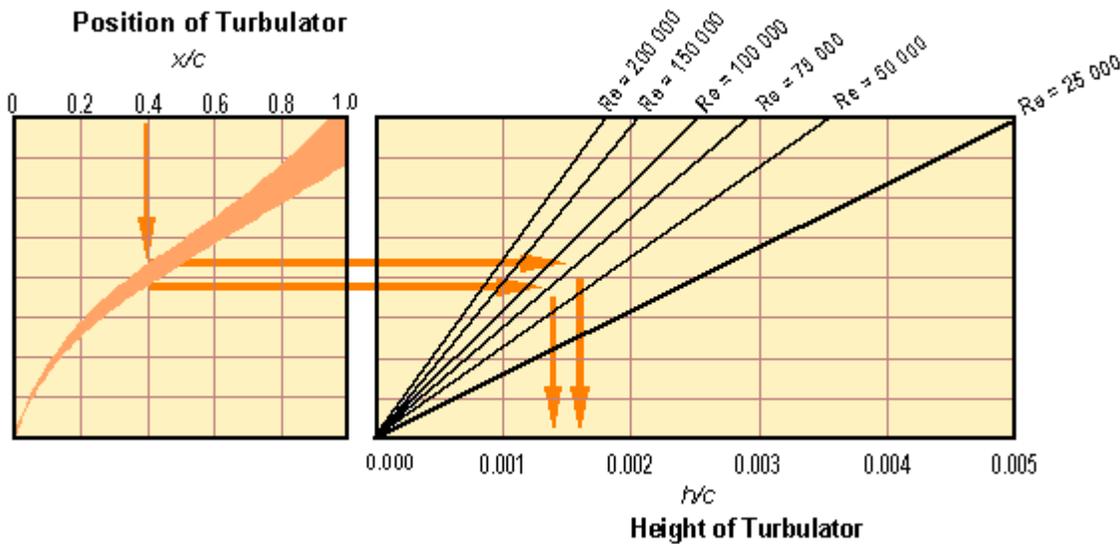
A typical mechanical turbulator consists of a strip of tape, attached to the wing surface. The chordwise position of the strip is depending on the airfoil shape. Of course it must be located in front of any laminar separation. The combined polar diagrams used on the airfoil data pages also contain the transition location, which can be considered the maximum downstream position of a turbulator; to be effective, a turbulator should be located 5 to 10% of the cord before this location. The polar diagram below shows how to find an initial location for experiments.



Plot of the transition location in the polar diagram.

For a selected lift coefficient of $Cl = 1.0$, we draw a horizontal line, which intersects the transition curve for the Reynolds number of interest. Moving down we can read the location from the x/c -axis. For the example, we find a value of $x/c = 0.45$, where laminar separation will occur, if no transition happened in front of this location. If necessary, a turbulator should be placed at $x/c = 0.4$ or further upstream. There is also a curve for the lower surface

(T.L.), which can be used to define a turbulator position for the lower surface, but this is usually only needed for airfoils with additional camber located close to the trailing edge, as found in some full scale sailplanes. A mechanical turbulator must have a certain minimum height to be effective. This height depends on the position of the device, because the boundary layer thickness is growing with increasing chord position. An additional parameter is the Reynolds number, which also influences the boundary layer thickness: high Reynolds numbers result in thinner boundary layers than small Reynolds numbers (at the same airfoil chord). The thickness of the transition strip must be sufficient to cause transition, but it should not be thicker than the boundary layer to avoid additional drag. Close to the leading edge the boundary layer is very thin (1/10s of a millimeter), when the flow reaches separation, it can grow much thicker (in the order of millimeters for model airfoils). The following diagram intends to help you by giving a first guess on the thickness of a turbulator.



Turbulator height selection chart.

You enter the chart (after selecting a x/c position for the turbulator from the polars or the recommendations of the airfoil) at the top left axis. Dropping a line down to the orange band gives an upper and a lower intersection point, from each of which you draw a straight line to the right, intersecting the line matching the Reynolds number corresponding to the wings chord length. On the axis below, the approximate boundary layer displacement thickness can be found and used as a first guess for the turbulator height. The values found from the graph agree reasonably well with wind tunnel results [25], but further experiments will be necessary to find the optimum height (if such a thing exists at all).

Example: A wing has a chord Reynolds number of $Re = 75\ 000$. The chord length is 200 mm. The airfoil designer recommends transition at $x/c = 0.4$ by means of a turbulator. Entering the graph with these values a turbulator height of 0.0014 to 0.0016 times chord, which evaluates to a thickness of 0.28 to 0.32 mm.

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MINUTES OF SOGGI MEETING APRIL 9 2000

The meeting was called to order by Bud Wallace at 2:05 PM. There were 17 members present. Minutes of the March 12 meeting were read by all.

ONE DESIGN CONTEST:

Stew Watson reported that Bird of Time kits could be purchased at Sunset Radio Control in Alberta for \$90.00 plus s&h.

NEW BUSINESS:

Bud Wallace stated that Old Timer Kits may be purchased from Stu Pierce in Barrie.

Werner Klebert said he was contacted by the representative of the Dundas Model Show about putting a glider in the show. Werner was concerned about enough space for his current model. The show is on Saturday April 15 at St. James church in Dundas.

Dick Francis who lives in Dundas repairs and checks out R-C radios.

The topic about protection when transporting model planes was discussed. To make wing covers use a foam cored soft cloth. This can be purchased at Lens Mills Store in Stoney Creek for about \$6.00 a pound.

FIELD:

There has been no word on when we can use the sod farm at this time.

Fred Freeman and Keith Armstrong installed a sign at the entrance to the field as to members only.

The flying out house had another short flight - no take off, just a crash. It will be returned to an upright position when flying commences.

CLUB DAY:

Werner Klebert will be the CD for the Club Day.

It was decided that the club would serve hot dogs and pop for this event. Bryn Rennie and Werner Klebert will look after purchasing the food. Bryn said he will supply a barbecue. It was suggested that T-Shirts be given as prizes for this event.

FLYING ACES:

Dick Fahey thanked the SOGGI members who gave a talk and demonstration to the Flying Aces at their meeting last month.

Memo from Dick Fahey:

2000 FLYING DATES - SQUADRON 40 - FLYING- ACES CLUB

8:00 A.M. TO 12:00 Noon: Saturdays.

May 6, May 20

June 3, June 17

July 1, July 29

Aug. 12, Aug.26

Sept. 9, Sept 23.

All field rules and codes of behavior will be observed by Squdn. 40 flyers.

1/ For access to the field, use the roadway on the East perimeter only, (refer to maps distributed last year).

2/ No driving or parking on sodded areas, parking permitted on the East side of tile roadway, facing North

Results:

Contestant	FreqCH		Round 1	Round 2	Round 3	Round 4	Total	Grand Total
Fred Freeman	22	Time	04:10	10:01	02:32	08:06	24:49	
		Adjusted	370	797	152	646	1965	
		Landing	0	0	0	0	0	1965
Albert Fund	49	Time	03:25	03:05	04:35	05:26	16:31	
		Adjusted	205	185	275	326	991	
		Landing	0	0	96	0	96	1087
Bryn Rennie	31	Time	01:59	03:03	03:44	08:10	16:56	
		Adjusted	317	183	284	610	1394	
		Landing	32	0	120	0	152	1546
Keith Armstrong	53.1	Time	02:00	06:26	02:33	04:49	15:48	
		Adjusted	320	394	153	289	1156	
		Landing	0	0	0	0	0	1156
Mike Kucera	26	Time	04:35	06:11	05:46	04:00	20:32	
		Adjusted	275	481	426	440	1622	
		Landing	56	0	0	0	56	1678
Larry Literovitch	48	Time	05:02	03:48	07:53	09:20	26:03	
		Adjusted	302	328	623	560	1813	
		Landing	40	0	168	0	208	2021
Derek Hartwell	11	Time	05:06	09:58	03:23	02:57	21:24	
		Adjusted	306	792	203	177	1478	
		Landing	0	0	0	0	0	1478
Dick Colley	22	Time	01:54	02:56	02:40	03:53	11:23	
		Adjusted	274	176	160	383	993	
		Landing	0	0	0	0	0	993
Otokar Koprinsky	23	Time	03:21	02:40	04:35	02:31	13:07	
		Adjusted	201	160	275	151	787	
		Landing	0	0	0	0	0	787
Cliff English	57	Time	01:30	01:36	04:49	01:58	09:53	
		Adjusted	90	108	289	312	799	
		Landing	0	0	0	0	0	799
Werner Klebert	50	Time	07:58	05:58	08:14	09:54	32:04	
		Adjusted	672	552	574	754	2552	
		Landing	88	120	56	56	320	2872
Bill Woodward	28	Time	04:00	07:48	05:11	03:41	20:40	
		Adjusted	440	568	311	251	1570	
		Landing	152	0	0	0	152	1722
Zivko Rizonko	52	Time	03:23	10:10	02:06	05:55	21:34	
		Adjusted	203	710	286	525	1724	
		Landing	0	0	0	0	0	1724

The restless wind appeared for the latter two rounds and gave most people trouble in seeking landing points, but when all the dust had settled it was Werner Klebert who reigned victorious, with Larry L. of GNATS in second place and Fred Freeman, with some steady flying, in third place.

No planes were lost, bent or damaged in any way so we all live to compete another day.

Mike Kucera flying a Pelikan demonstrated what a zoom start can look like (try one of those with a Bird of Time!) and also how hard it is to see these sleek birds when they are edge on.

Larry Literovich on behalf of GNATS extended an invitation to any of our members to attend a Novathon, June 25th and an Open Thermal Duration Contest on August 6th, both to be held at Fenwick (see the MAAC Mag for more info)

**Is there anybody out there? – Who has an article inside just bursting to get out
- We publish for free!**

For Sale: Want Ads: Personals

For Sale:

Bird of Time – Some(More) Impact Damage, ~~not~~ even good for Spare Ribs
(Barbeque fuel)

Plus ~~23~~ 12 sheets of 150 grit emery cloth (well worn – not good for lining cat litter boxes),
Charred Hair-piece and ~~three~~ one finger splints (FREE to good home)

For more Information Call: Harry 'Nails' Kneelson (360)-779-123

Wanted:

Gentle Lady or similar Docile Glider suitable for beginner Pilot.
Dust off those old collectibles and help a youngster discover the joy of soaring.

Contact: Bryn Rennie (905)-385-3365



The Southern Ontario Glider Group is a chartered club of MAAC

1999 SOGGI Executive

President:	Bud Wallace 1060, Eastmount Avenue Mississauga, Ont. L5E 1Z3	905-274-3177
Vice President:	Werner Klebert 69, Byron Avenue Stoney Creek, Ont. L8J 2T1	905-578-9431
Treasurer:	Derek Hartwell 39, Isaac Brock Drive Stoney Creek, Ont. L8J 2P1	905-578-7991
Secretary:	Cliff English 24, Blackwood Crescent Hamilton, Ont. L8S 3H5	905-522-4561
Editor:	Dick Colley 101, Braeheid Avenue Waterdown, Ont. L0R 2H5	905-689-7761

Deadline for June Issue of Task: May 22nd 2000

2000 Calendar of Events

- June 1-30 B-O-T Postal Contest CD Stan Shaw (See March Minutes)
- June 4 Optional Triathlon CD Cliff English
- June 11 Golden Oldies CD BudWallace
- June 18 One Design Phase 2 CD Bud Wallace/Cliff English
- July 9 One Design Phase 3 CD Bud Wallace/Cliff English
- July 16 Otto Bandman Club Day CD Werner Klebert
- (Re-scheduled event)
- Aug 13 One Design Phase 4 CD Bud Wallace/Cliff English
- Aug 27 Novathon CD Fred Freeman
- Sept 3 Big Bird Bash CD Werner Klebert/K. Armstrong
- Sept 17 One Design Phase 5 CD Bud Wallace/Cliff English
-

TASK**MEMBERSHIP LIST**

Keith	Armstrong	219, Governors Road	DUNDAS	Ont	L9H 3J7	905-627-4011
Peter	Ashton	200, Edwin Street	Kitchener	Ont	N2H 4P2	519-576-6750
Roy	Auwaerter	9, Jamieson Drive	DUNDAS	Ont	L9H 5A1	905-627-8496
Joseph	Baltaza	19, Gaitwin Street	Brantford	Ont	N3P 1A9	519-751-3698
Robert	Batt	612, Blue Forrest Hill	Burlington	Ont	L7L 4H3	905-632-8790
Rob	Campbell	34, Hopkins Court	DUNDAS	Ont	L9H 5M5	905-627-9435
Dick	Colley	101, Braeheid Avenue	WATERDOWN	Ont	L0R 2H5	905-689-7761
Cliff	English	24, Blackwood Crescent	HAMILTON	Ont	L8S 3H5	905-522-4561
Fred	Freeman	511-120 Strathcona Ave N	HAMILTON	Ont	L8R 3J5	905-525-6509
Albert	Fund	73, Beech Street	CAMBRIDGE	Ont	N3C 1X6	519-658-9495
Arnold	Gardner	202, San Pedro Drive	HAMILTON	Ont	L9C 2E1	905-383-4418
Don	Guthrie	RR4	Belwood	Ont	N0B 1J0	519-843-4537
Bob	Hammett	183, Uplands Drive	KITCHENER	Ont	N2M 4X3	519-576-7636
Derek	Hartwell	39, Isaac Brock Drive	Stoney Creek	Ont	L8J 2P1	905-578-7991
Werner	Hildesheim	4, Foster Crescent	CAMBRIDGE	Ont	N1R 4R1	519-623-2663
Herb	Jenkins	238, Lloyinn Ave.,	ANCASTER	Ont	L9G 1J1	905-648-6123
Werner	Klebert	59, Byron Avenue	STONEY CREEK	Ont	L8J 2T1	905-578-9431
Otakar	Koprnicky	75, Hazelwood Crescent	CAMBRIDGE	Ont	N1R 8A4	519-740-9504
Herb	Lentfer	23, Walsh Court	BRANTFORD	Ont	N3T 5Y1	519-753-2856
Jack	Linghorne	55, Angelsey Boulevard	ISLINGTON	Ont	M9A 3B8	416-233-0230
Ken	Lockwood	29, Cross Creek Blvd.,	Guelph	Ont	N1H 6J2	519-821-9947
Tom	McCann	2206, Townline Crescent	OAKVILLE	Ont	L6H 5H4	905-257-2101
Mike	Penney	388, Massey Drive	ANCASTER	Ont	L9G 3J9	905-648-5843
Paul	Penney	388. Massey Drive	ANCASTER	Ont	L9G 3J9	905-648-5843
Bryn	Rennie	22/1255 Upper Gage Avenue	HAMILTON	Ont	L8W 3C7	905-385-3365
Zivko	Rizoniko	479, Fendalton Street	MISSISSAUGA	Ont	L5B 2L8	905-275-0597
Ann	Tekatch	19, Pheasant Place	Hamilton	Ont	L9A 4Y4	905-575-5433
Bob	Thayer	4108, Millcroft Park	BURLINGTON	Ont	L7M 3V9	905-336-3290
Mike	Thomas	61, Alhart Drive	ETOBICOKE	Ont	M9V 2N1	416-748-2833
Walter	Tremmel	56-600 Silvercreek Blvd	MISSISSAUGA	Ont	L5A 2B4	905-270-5959
Juri	Vosu	3291, Candela Drive	MISSISSAUGA	Ont	L5A 2V1	905-279-9549
Bud	Wallace	1060, Eastmount Avenue	MISSISSAUGA	Ont	L5E 1Z3	905-274-3177
Stewart	Watson	26, Juanita Drive	HAMILTON	Ont	L9C 2G3	905-385-8214
Doug	Wilkins	8448, Twenty Road	HAMILTON	Ont	L9B 1H7	905-679-4973
Bill	Woodward	520, Pine Street	Cambridge	Ont	N3H 2S6	519-653-4251

Correction Notice:

NAME:
 ADDRESS:
 CITY/TOWN:
 POSTAL CODE:
 PHONE:
 e-mail:

